

#### 470-10-06

**DATE:** October 14, 2010

- **SUBJECT:** Update to Publication 148 (Traffic Standards Signals [TC-8800 Series]) and Publication 149 (Traffic Signal Design Handbook), Chapter 20 "Criteria for the Design of Traffic Signal Supports"
- TO:District ExecutivesR. Craig Reed, Director, Bureau of Municipal Services
- FROM: R. Scott Christie, P.E. /s/ Deputy Secretary for Highway Administration

This Strike-Off letter is time neutral but will result in increased material costs to meet fatigue design requirements and bring PennDOT in conformance with the most recent release of the American Association of State Highway and Transportation Officials (AASHTO) standard specifications, the Manual on Uniform Traffic Control Devices, and the National Electric Code.

The accompanying revisions to Publication 148 (Traffic Standards – Signals [TC-8800 Series]) and Publication 149 (Traffic Signal Design Handbook), Chapter 20 "Criteria for the Design of Traffic Signal Supports" become effective immediately, for all traffic signal structural supports as follows:

- All Department projects submitting Plans, Specifications, and Estimate packages to Central Office.
- All Highway Occupancy Permits or Municipal projects that do not have an approved Traffic Signal Permit.

This Strike-Off letter also applies to any traffic signal structural support that requires replacement. An exemption to this requirement will be considered only when the following conditions are met:

- The affected municipality has an existing stockpile of NEW traffic signal structural supports purchased prior to this Strike-Off letter.
- The municipality provides verification (signed and sealed from a Professional Engineer, licensed in the State of Pennsylvania) attesting to the structural adequacy of the existing foundation and the suitability of the stockpiled signal support material for its intended use and location.
  - A modified base plate configuration as indicated in "Attachment A" will be required.

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In addition to the revisions made to the standards, Publication 35, Bulletin 15 - Approved Construction Materials, Section 1104.02 will also be updated accordingly to indicate those manufacturers who have been re-certified to provide traffic signal supports meeting the new criteria. Drawings for the approved manufacturers are available for Department representatives at: <a href="http://ftp.dot.state.pa.us/transfer/Traffic Signals/Traffic Signal Structrual Supports/">http://ftp.dot.state.pa.us/transfer/Traffic Signals/Traffic Signal Structrual Supports/</a>.

The Department is implementing the changes to Publication 408 (Specifications) for use immediately on projects, via a Standard Special Provision (Attachment B). These revisions will be permanently incorporated into Publication 408 with the October 2010 update.

These changes have been developed through a collaborative effort involving the Bureau of Highway Safety and Traffic Engineering (BHSTE), the Bureau of Design, the Bureau of Construction and Materials, along with existing Bulletin 15 approved traffic signal support manufacturers.

If you have any questions regarding the attached updates, please contact Glenn C. Rowe, P.E., PTOE, Chief, Transportation Operations Division, BHSTE at (717) 783-6479.

#### Attachments

CC: FHWA Pennsylvania Division Office Pennsylvania State Association of Township Supervisors Pennsylvania State Association of Boroughs Pennsylvania State Association of Township Commissioners Pennsylvania League of Cities and Municipalities Director, Policy Office Highway Administration Bureau Directors Assistant District Executives **District Traffic Engineers District Bridge Engineers** District Permit Managers **District Plans Engineers** Bureau of Highway Safety and Traffic Engineering Division Chiefs Bureau of Design Division Chiefs Bureau of Construction Materials Division Chiefs G. Gordon, P.E., 7th Floor CKB J. Unick, P.E., 7th Floor CKB D.T. Wilhelm, P.E., Materials Testing Lab J. A. Bracken, P.E., Materials Testing Lab

4700/DPF/(3-0333)/lap/(7-3620)/tns(7-7350)

BCC: Directors Correspondence File TOD Read File





## SECTION 1104—TRAFFIC SIGNALS

## **Revise Section 1104.01 – General Requirements to add the following:**

(b) Structural Material. Fabricate traffic signal structural material according to Section 1105 (steel members only), the American Welding Society (AWS), and the American Association of State Highway and Transportation Officials (AASHTO) Specifications; except, applying water to the base metal during plasma arc cutting is permitted. <u>Bulletin 15</u> listing and shop inspection is required. Fabricators provide an AWS certified welding inspector (CWI) for welded steel or aluminum pole products as specified in Section 1105.01(g)3. <u>Bulletin 15</u>, shop inspection, and Section 1105 do not apply to painting of aluminum poles and for the following non-welded items: cast aluminum poles, cast steel poles, and cast iron poles.

The Charpy V-Notch toughness test is required for load carrying tension members greater than 13 mm (1/2-inch) in thickness, as required for Zone 2, non-fracture critical criteria, of the applicable AASHTO specifications.

Provide steel poles that either round or multi-sided with a minimum of eight sides.

Provide testing and test methods according to AWS D1.1 (Steel) or AWS D1.2 (Aluminum) and as determined by the Materials Testing Division (MTD).

Provide non-destructive testing on 100% of full penetration groove welds and a random 25% of partial penetration groove welds of longitudinal seams on steel poles and arms. When inspecting full penetration seam welds, use radiographic test methods on material less than 8 mm (5/16-inch) in thickness, and use radiographic or ultrasonic test methods on material 8 mm (5/16-inch) and greater in thickness. Use magnetic particle inspection on partial penetration seam welds.

Provide non-destructive testing by ultrasonic test methods on random 25% of all pole to base plate and arm to arm plate full penetration groove welds. For tube material less than 8 mm (5/16-inch) in thickness, have the fabricator submit a detailed ultrasonic testing procedure, including acceptance criteria, to the MTD for review and approval before testing.

For all other welds on steel traffic poles, perform magnetic particle inspection on a minimum of 25% of the length of each weld. Provide inspection for the full length of the weld when less than 150 mm (6 inches) in length. For aluminum traffic pole structures, perform fabrication and non-destructive testing in accordance with Section 1101.01.

Where less than 100% of the weld is non-destructively tested, and a rejectable defect is found, test 100% of the length of the weld.

Where applicable, the Department's plant inspector will select portions of welds to be tested. Perform and evaluate all non-destructive testing according to cyclically loaded non-tubular tension criteria.

(c) Certification. As specified in Section 106.03(b)3. Certify from the manufacturer, that all signal supports satisfy the Department's criteria and are adequate to support the loads indicated on the approved plans. Include on the certification the signature and seal of a Professional Engineer registered in the State. Certify the structural adequacy of all sign and signal brackets as well as all other mounting hardware.

## **Revise Section 1104.02 – Traffic Signal Supports to read as follows:**

## 1104.02 TRAFFIC SIGNAL SUPPORTS—

## (a) General.

1. **Design and Acceptance.** Design in accordance with Publication 149. Submit shop drawings in accordance with Publication 149, including calculations for all special structures, for review and acceptance.

## 2. Supports.

Fabricate shafts and arms in any of the following shapes and styles:

## A. Round Tapered.

- i. One longitudinal seam, continuously welded, and ground or rolled flush.
- ii. Transverse butt welds are not acceptable.
- iii. Uniform wall thickness.
- iv. Uniform taper, 11.7 mm (0.14 inch) maximum and 5.8 mm (0.07 inch) minimum per meter (foot) of length.

## **B.** Round Stepped.

- i. Round pipe sections, each with not more than one longitudinal seam continuously welded and ground or rolled flush. Join sections by a hot-swaged shrink fit continuously seal-welded to prevent entrance of water.
- ii. Uniform wall thickness for each section.
- Maximum change in diameter between stepped sections not to exceed 54 mm (2 1/8 inches).

## C. Multi-Sided Tapered.

- i. Maximum of two longitudinal seams, continuously welded, and ground or rolled to a maximum bead height of 3.2 mm (1/8 inch).
- ii. Transverse butt welds are not acceptable.
- iii. Uniform wall thickness.
- iv. Uniform taper, 11.7 mm (0.14 inch) maximum and 5.8 mm (0.07 inch) minimum per meter (foot) of length.
- v. Minimum of eight sides.

## **D. Round Untapered.**

- i. Maximum of one longitudinal seam, continuously welded, and ground or rolled flush.
- ii. Uniform wall thickness and diameter.
- iii. Transverse butt welds are not acceptable.

- 3. Cable Support. Weld a cable support to the inside top of the shaft.
- 4. **Grounding.** Weld a UL-Listed grounding lug, capable of accommodating a 13.3 mm<sup>2</sup> (No. 6 AWG) stranded copper cable, to the inside of the shaft adjacent to the handhole.
- 5. **Handholes.** Provide a handhole in the shaft of the poles, as shown on the <u>Standard</u> <u>Drawings</u>. Reinforce the area to develop the minimum guaranteed yield strength of the shaft. Furnish a cover and keeper chain.
- 6. Wire Inlets. Provide a wire inlet at each signal head or at each electrically operated sign location. Weatherproof each inlet with an insulated grommet. Provide a deburred hole, 63.5 mm (2 1/2-inch) minimum diameter, in the flange plate and shaft, which serves as a wire entrance into the arm from inside the shaft. Provide Type LB access fittings from Type II mounted controller cabinet into pole shaft and in pole shafts for pedestrian pushbuttons.

## 7. Anchor Bases.

- A. Fabricate the base clean, smooth, and of the dimensions necessary for adequate pole mounting and structural support.
- B. Provide holes for anchor bolts.
- C. Fabricate the base to telescope over the shaft and be secured in place by welding.
- 8. Galvanizing. Section 1105.02(s) and as follows:
  - A. Galvanize steel shafts and arms, including those manufactured of high strength and corrosion resistant steels, according to the American Society of Testing Materials (ASTM) A 123 (AASHTO M 111). Galvanize accessories and hardware according to ASTM A 153 (AASHTO M 232).
  - B. **Overhead Supports.** As shown on the <u>Standard Drawings</u> and as follows:
    - i. Shaft and Arms—AASHTO M270/ASTM A709, Grade 36 or Grade 50, ASTM A36, ASTM A 53, ASTM A 572 Grade 50, ASTM A 501 and A 595.
    - ii. Luminaire Mounting Arms—Section 1101.03.
    - iii. Anchor (Base) Plates, Flange (Arm and Column Connection) Plates, and Gusset Plates,—AASHTO M 270 (ASTM A 709), Grade 36. ASTM A 36, ASTM A 572 Grade 50.
    - iv. Miscellaneous Shapes, plates and bars- AASHTO M 270 (ASTM A 709), Grade 36. ASTM A 36, ASTM, ASTM A 572 Grade 50 and ASTM A992.
    - v. Flange Plate Assembly Bolts, Nuts and Washers— ASTM A325, ASTM 563 and ASTM F436. Mechanically galvanize in accordance with ASTM B695. Furnish bolts, nuts and washers for testing purposes and test as specified in Section 1050.3(c) 7.b.
    - vi. Shaft and Arm Caps—Galvanized steel (C-coat) cast iron or cast aluminum.
  - vii. Handhole CHandhole Cover Plates AASHTO M 270 (ASTM A 709), Grade 36. ASTM A 36, ASTM, ASTM A 572 Grade 50 and ASTM A 1011.

- viii. Pipe Caps AASHTO M 270 (ASTM A 709), Grade 36. ASTM A 36, ASTM, ASTM A 572, ASTM A 1011 or ASTM B 26.
- ix. Arm dampening Harmonic dampening device, when provided.
- C. Pedestal Supports. As shown on the <u>Standard Drawings</u> and as follows:

## i. Aluminum.

- a. Support—One length, 114 mm (4 1/2-inch) minimum outside diameter aluminum pipe, Schedule 40, ASTM B 210, or B 221, Alloy 6063-T6.
- b. Bases—Cast aluminum, ASTM B 26, or B 108, Alloy 356-T6; aluminum plate, ASTM B 209, Alloy 6061-T6.
- c. Pole Tops—Aluminum.
- ii. Steel.
  - a. Support—One length, 114 mm (4 1/2-inch) minimum outside diameter steel pipe, Schedule 40, ASTM A 53, Type F.
  - b. Base—Steel casting, ASTM A 27, Grade 65-35; gray iron casting, ASTM A 126, Class 26; steel plate, AASHTO M 270 (ASTM A 709), Grade 36.
- D. **Pedestrian Stub Poles.** As specified in Section 1104.02(c) except having a fixed length of 1,500 mm (60 inches) and a rounded top cap to minimize injuries.
- E. Anchor Bolts. As shown on the <u>Standard Drawings</u> and as follows:
  - i. Anchor Bolts—ASTM A 449 or F 1554.
  - ii. Hex Nuts—ASTM A 563M/A 563.
  - iii. Washers—ASTM F 436.

Galvanize the top 200 mm (8 inches) of bolts and all associated hardware as specified in Section 1105.02(s) (ASTM A 153), or by another acceptable method conforming to the coating thickness, adherence, and quality requirements of ASTM A 153. Furnish template prints for setting anchor bolts with each support.

- F. **Wood Support Poles.** When used for temporary signal installations, certify sawn material, both rough and dressed by the mill as to grade and mark in accordance with the grading rules and basic provisions of the American Lumber Standards (PS-20-70) by a lumber grading or inspection bureau or agency. If dressed, the grade mark shall be applied after dressing.
- G. Span Wire. ASTM A 475, Class A, Siemens-Martin, or ASTM B 416.
- H. Tether Wire. ASTM A 475, Class A, Siemens-Martin, or ASTM B 416.
- I. Lashing. As shown on the <u>Standard Drawings</u> for attaching cable to span wire.

OS-299 (7-08)	TRANSMITT	AL LETTER	PUBLICATION: 148 DATE: 10/14/2010			
SUBJECT:						
Tr	affic Standards - Sig	Inals (TC-8800 Se	eries)			
INFORMATION AND SPEC	IAL INSTRUCTIONS	:				
Conformance with the 2001 (AASHTO) "Standard Specific Signals" including interim sp Devices 2009 Edition, and th The accompanying re and Publication 149 (Traffic Signal Supports", for all traffic • All Department project Office. • All Highway Occupant Signal Permit. • For any traffic signal exemption to this req o The affected m supports purc o The municipal licensed in the existing found intended use A modi	American Association cations for Structural S ecifications up to 2006 the National Electric Coo visions to Publication S Signal Design Handboo fic signal structural sup cts submitting Plans, S cy Permits or Municipal structural supports that uirement will be consider hased prior to this Structural hased prior to this Structural ity provides verification to the suitability and location. fied base plate configu- ed.	of State Highway a Supports for Highway b, the national Man de 2008 Edition. 148 (Traffic Standa ok), Chapter 20 "Cr oports as follows: Specifications, and I I projects that do n at require either ren dered only when the sting stockpile of N ike-off letter. n (signed and seale a) attesting to the s ty of the stockpiled iration as indicated	nd Transportation Officials ay Signs, Luminaires and Traffic ual on Uniform Traffic Control ards – Signals [TC-8800 Series]) riteria for the Design of Traffic Estimate packages to Central not have an approved Traffic moval or replacement. An the following conditions are met. NEW traffic signal structural ed from a Professional Engineer, structural adequacy of the l signal support material for its in "Attachment A" will be			
CANCEL AND DESTROY TH This will replace the June 19 (Traffic Standards - Signals and the September 1988 "Cr of Traffic-Related Structures Publication 149 (Traffic Sign Handbook), Chapter 20) on t	<b>HE FOLLOWING:</b> 89 Publication 148 (TC-7800 Series)) riteria for the Design " (currently al Design the effective date.	ADDITIONAL COFROM:	DPIES ARE AVAILABLE LES STORE 246 phone 279 fax lesstore.state.pa.us osite - www.dot.state.pa.us <i>hs, Publications &amp; Maps</i> use (PennDOT employees ONLY)			

## APPROVED FOR ISSUANCE BY:

Allen D. Biehler, P.E. Secretary of Transportation By:

Daryl Sr. Chi

Daryl St. Clair, P.E. Acting Director, Bureau of Highway Safety and Traffic Engineering



# **INDEX OF TRAFFIC STANDARDS – SIGNALS**

STANDARD DRAWING NO	D. DATE	DESCRI
TC-8801 (7 SHEETS)	October 14, 2010	TRAFFIC SIG
TC-8802	October 14, 2010	CONTROLLER
TC-8703 (2 SHEETS)	October 14, 2010	MISCELLANEC
TC-8804 (2 SHEETS)	October 14, 2010	ELECTRICAL
TC-8805	October 14, 2010	SIGNAL HEAD
TC-8806 (2 SHEETS)	October 14, 2010	DETECTORS

- IPTION
- GNAL SUPPORT
- ASSEMBLY
- OUS
- DISTRIBUTION
- DS



NOTES:

- 1. FOR FOUNDATION DETAILS, SEE SHEETS 3 THROUGH 5.
- 2. PLACE HANDHOLE 90° OR 180° FROM CENTERLINE OF ARM "A".
- 3. DIMENSION "K" IS FROM SIDEWALK. IF NO SIDEWALK, DIMENSION "K" IS FROM PAVEMENT GRADE AT CENTER OF ROADWAY. PROVIDE SPECIFIED DIMENSION "K" SUCH THAT CLEARANCE IS IN THE RANGE OF: 8' MINIMUM, 15' MAXIMUM FOR TRAFFIC SIGNAL HEADS; 7' MINIMUM, 10' MAXIMUM FOR PEDESTRIAN SIGNAL HEADS.
- 4. DIMENSION "F" IS 2' MINIMUM FROM CURB OR FROM EDGE OF SHOULDER. PLACE POST-MOUNTED SIGNALS 2' MINIMUM BEHIND CURB OR EDGE OF SHOULDER.
- A "ROUND TAPERED" SUPPORT IS USED FOR ILLUSTRATION PURPOSES. THE TYPE OF SUPPORT MAY BE ANY OF THOSE INDICATED IN PUBLICATION 408.
- 6. INSTALL A MINIMUM OF ONE GROUND ROD AT EACH FOUNDATION. SEE TC-8804.
- 7. ARMS LESS THAN 31' WILL BE ONE SECTION.
- RIGIDLY MOUNT ALL SIGNAL HEADS ON THE MAST ARM UNLESS OTHERWISE INDICATED. PROVIDE MOUNTING BRACKETS THAT:
- a. ATTACH TO THE TOP AND BOTTOM OF THE SIGNAL HEAD. FOR 5-SECTION HEADS, ATTACH EITHER TO THE TOP AND BOTTOM OF THE SIGNAL HEAD, OR TO THE BOTTOM AND BETWEEN THE RED AND YELLOW SECTIONS OF THE SIGNAL HEAD.
- b. PERMIT THE ADJUSTMENTS SHOWN IN DETAIL A.
- c. HAVE GROMMETED WIRE ENTRANCE.
- d. DO NOT ENTRAP WATER INSIDE THE BRACKET.
- OBTAIN ELEVATION OF ROADWAY AND TOP OF FOUNDATION PRIOR TO DETERMINING THIS DIMENSION.
- PROVIDE SPECIFIED CLEARANCE IN ACCORDANCE WITH PUBLICATION 149 AND "THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES".
- 11. USE ONE-PIECE SHAFT WHEN LUMINAIRE IS REQUIRED EXCEPT FOR ROUND STEPPED SUPPORTS, OR UNLESS ALTERNATE OVERLAP SLIP JOINT IS SPECIFIED OR APPROVED ON A PROJECT-BY-PROJECT BASIS.
- 12. IF SPECIFIED, PROVIDE 36" MINIMUM STUB TO ALLOW FUTURE LUMINAIRE ATTACHMENT VIA OVERLAP SLIP JOINT.
- 13. FOR MAXIMUM ALLOWABLE DIMENSION "Y", SEE THE DEPARTMENT'S "CRITERIA FOR THE DESIGN OF TRAFFIC SIGNAL SUPPORTS", PUBLICATION 149.
- 14. FOR QUANTITY, SIZE, SIZE OF HOLES AND BOLT CIRCLE FOR ANCHOR BOLTS, SEE SHEET 3.
- FOR ANCHOR BOLTS, SEE SHEET 3.
  15. DURING 30-DAY TEST PERIOD, VISUALLY INSPECT NEW MAST ARM INSTALLATION FOR GALLOPING IN 5 TO 20 MPH WIND CONDITION. CONTINUE VISUAL INSPECTION FOR ANOTHER 180-DAY PERIOD AS INDICATED IN PUB. 408. PROVIDE GALLOPING MITIGATION DEVICE AS RECOMMENDED BY THE FABRICATOR AND APPROVED BY THE OWNER IF THE MAXIMUM DISPLACEMENT (MAX. POSITIVE TO MAX. NEGATIVE) AT THE MAST ARM TIP EXCEEDS 8". IF A MITIGATION DEVICE IS INSTALLED, CONTINUE VISUAL INSPECTION OF MAST ARM FOR THE ABOVE CRITERIA DURING 180-DAY PERIOD. PROVIDE VISUAL INSPECTION RECORDS TO THE OWNER AT THE END OF THE 180-DAY PERIOD. GALLOPING MAY RESULT IN LARGE AMPLITUDE, RESONANT OSCILLATIONS IN A PLANE NORMAL TO THE DIRECTION OF WIND FROM UNQUE COMBINATIONS OF ATTACHMENT GEOMETRY, ATTACHMENT ORIENTATION, ATTACHMENT WEIGHTS, WIND DIRECTION AND STRUCTURE STIFFNESS.



RECOMMENDED Oct.14,2010	RECOMMENDED Oct.14,2010	SHEET 1 OF 7
CHIEF, TRANSPORTATION OPERATIONS DIVISION	ACTING DIR. BUR. OF HIGHWAY SAFETY AND TRAFFIC ENGINEERING	TC-8801



#### ANCHOR BOLT DESIGN TABLE, MAST ARM

HIGT IDV			ONE	ARM		TWO ARMS *			
LENGTH (FT)	QTY.	DIA. (IN)	LGTH. (FT)	B.C. (IN)	HOLE (IN)	DIA. (IN)	LGTH. (FT)	B.C. (IN)	HOLE (IN)
0 - 10	6	1 3⁄4 "	**	18 "	2 "	1 3⁄4 "	**	18 "	2 "
>10 - 15	6	1 3⁄4 "	**	18 "	2 "	1 3⁄4 "	**	18 "	2 "
>15 - 20	6	1 3⁄4 "	**	18 "	2 "	1 3⁄4 "	**	18 "	2 "
>20 - 25	6	1 3⁄4 "	**	18 "	2 "	1 3⁄4 "	**	18 "	2 "
>25 - 30	6	1 3⁄4 "	**	21"	2 "	1 3⁄4 "	**	21 "	2 "
>30 - 35	6	1 3⁄4 "	**	21"	2 "	1 3⁄4 "	**	21 "	2 "
>35 - 40	6	2 "	**	24 "	21/4 "	2 "	**	24 "	21/4 "
>40 - 45	6	2 "	**	24 "	21/4 "	2 "	**	24 "	21/4 "
>45 - 50	6	2 "	**	24 "	21/4 "	2 "	**	24 "	21/4 "
>50 - 60	6	2 "	**	24 "	21/4"	2"	**	24 "	21/4"

#### ANCHOR BOLT DESIGN TABLE, STRAIN POLE

DESIGN		SHAF	T LENGT	FH 20′ -	24′	SHA	FT LENG	TH 26′	- 30′	SHAF	T LENGT	H 32′ -	34′
(LBS)	QTY.	DIA. (IN)	LGTH. (FT)	B.C. (IN)	HOLE (IN)	DIA. (IN)	LGTH. (FT)	B.C. (IN)	HOLE (IN)	DIA. (IN)	LGTH. (FT)	B.C. (IN)	HOLE (IN)
1000	6	1 3⁄4 "	**	18 "	2 "	2 "	**	18 "	21/4 "	2 "	**	18 "	21/4 "
2000	6	1 3⁄4 "	**	18 "	2 "	2 "	**	18 "	21/4 "	2 "	**	18 "	21/4 "
3000	6	1 3⁄4 "	**	18 "	2 "	2 "	**	18 "	21/4 "	2 "	**	18 "	21/4 "
4000	6	1 3⁄4 "	**	18 "	2 "	2 "	**	18 "	21/4 "	2 "	**	18 "	21/4 "
5000	6	1 3⁄4 "	**	18 "	2 "	2 "	**	18 "	21/4 "	2 "	**	18 "	21/4 "
6000	6	21/4 "	**	18 "	21/2 "	21/4 "	**	21 "	21/2 "	21/4 "	**	21 "	21/2 "
7000	6	21/4 "	**	18 "	21/2 "	21/4 "	**	21 "	21/2 "	21/4 "	**	21 "	21/2 "
8000	6	21/4 "	**	18 "	21/2 "	21/4 "	**	21"	21/2 "	21/4 "	**	21 "	21/2 "
9000	6	21/4 "	**	18 "	21/2 "	21/4 "	**	21"	21/2 "	21/2 "	**	21"	2 3⁄4 "
10.000	6	21/4"	**	18 "	21/2"	21/4 "	**	21"	21/2 "	21/2 "	**	21"	23/4"

\* TWO ARMS PERPENDICULAR TO EACH OTHER. ADDITIONAL STRUCTURAL ANALYSIS IS REQUIRED FOR TWO MAST ARMS AT ACUTE OR OBTUSE ANGLES TO EACH OTHER

\*\* FOR FOUNDATION TYPE A, ANCHOR BOLT LENGTH IS 6'. FOR FOUNDATION TYPE B, ANCHOR BOLT LENGTH IS EQUAL TO "Y" OR "Z" DEPTHS MINUS 6" B.C. = BOLT CIRCLE DIAMETER



DESIGN CRITERIA		(SEE NOTE 13)
ALL MAIN LOAD CA MUST MEET AASHTO CHARPY V-NOTCH (1	RRYING TENSION MEMBERS ZONE 2, NON-FRACTURE CVN).	GREATER THAN $\frac{1}{2}$ INCH THICKNESS CRITICAL MEMBER COMPONENTS (FCM)
EXTERNAL LOADS		AASHTO SIGN SPEC †
ICE LOAD WIND LOAD		SECTION 3.7 APPENDIX C, SECTION C.3, EQ. C-1, WITH 80 MPH WIND AND 30% GUST FACTOR
GROUP LOADS		aashto sign spec section 3.4 $^{\dagger}$
BOLT CRITERIA		AASHTO SIGN SPEC <sup>†</sup>
BOLT CRITERIA ALLOWABLE ANCHOR	BOLT STRESSES	SECTION 5.16 SECTION 5.17
SPREAD FOOTINGS		
MAXIMUM DESIGN P MINIMUM AREA IN UNIT WEIGHT OF S	RESSURE BEARING DIL	1.5 TONS PER SQUARE FOOT 100% 100 POUNDS PER CUBIC FOOT
DRILLED SHAFTS (	CAISSONS)	DM4 SECTION 10.7.3.8.2P
MAXIMUM DESIGN P MAXIMUM DESIGN L MODULUS OF SUBGR ABOVE BELOW WATER TABLE UNIT WEIGHT OF S ANGLE OF INTERNA COHESION	RESSURE ATERAL DISPLACEMENT ADE REACTION: WATER TABLE WATER TABLE DIL _ FRICTION	1.5 TONS PER SQUARE FOOT O.5" K = 60.0 POUNDS PER CUBIC INCH K = 40.0 POUNDS PER CUBIC INCH 3 FEET BELOW GRADE 120 POUNDS PER CUBIC FOOT 25° 0 KIPS PER SQUARE FOOT
LEGEND		
AASHTO SIGN SPEC:	AMERICAN ASSOCIATION "STANDARD SPECIFICATI LUMINAIRES AND TRAFFI SPECIFICATIONS (2002,	OF STATE HIGHWAY AND TRANSPORTATION OFFICI ONS FOR STRUCTURAL SUPPORTS FOR HIGHWAY SI C SIGNALS", 4TH EDITION (2001) INCLUDING I , 2003 AND 2006)
DM4:	PENNSYLVANIA DEPARTME SEPT. 2007 (INCLUDING	NT OF TRANSPORTATION, DESIGN MANUAL PART 4 Change no.1 dated june 2009)
U. N. O. :	UNLESS NOTED OTHERWIS	E

#### FOUNDATION NOTES:

- PROVIDE 3" CONCRETE COVER ON REINFORCEMENT BARS, EXCEPT AS NOTED.
- USE CLASS A CEMENT CONCRETE f'c = 3000 PSI IN PEDESTALS, FOOTINGS AND CAISSONS.
- PROVIDE GRADE 60 REINFORCING STEEL BARS THAT MEET THE REQUIREMENTS OF ASTM A615/A615M-96A FOR CONCRETE REINFORCEMENT. DO NOT WELD REINFORCING STEEL BARS.
- RAKE-FINISH ALL HORIZONTAL CONSTRUCTION JOINTS, EXCEPT AS INDICATED.
- 5. CHAMFER EXPOSED CONCRETE EDGES 1 " × 1 ".
- 6. DIMENSIONS ARE BASED ON A NORMAL TEMPERATURE OF 20°C (68°F).
- GALVANIZE ALL STRUCTURAL STEEL IN ACCORDANCE WITH PUB. 408, SECTION 1104.02 (d) 9.
- 8. PROVIDE ANCHOR BOLT HOLES  $^{1}\!/_{4}$  " LARGER THAN BOLT DIAMETER.
- PROVIDE ANCHOR BOLTS CONFORMING TO ASTM F1554 GRADE 55 PER PUBLICATION 408, SECTION 1105.02 (c) 3.
- 10. USE STEEL TEMPLATE TO SET ANCHOR BOLTS IN ACCORDANCE WITH PUBLICATION 408, SECTION 1104.02 (d).
- 11. STEEL TEMPLATE TO BE PROVIDED BY MAST ARM OR STRAIN POLE FABRICATOR.
- 12. PROVIDE ANCHOR BOLTS WITH THREADS WHICH EXTEND A MINIMUM OF 3" BELOW THE TOP OF THE FOUNDATION.
- 13. SEE PENNDOT PUBLICATION 149 "CRITERIA FOR THE DESIGN OF TRAFFIC SIGNAL SUPPORTS".



FOUNDATI	ON FOR 1	[RAFFIC ]	SIGNAL S	UPPORT,	MAST ARM
MAST ARM	"D "	н (	FT)	"W "	BAR
(FT)	(FT)	ONE ARM	TWO ARMS*	QTY.	SIZE
0 - 10	3′-0 "	10′-0"	10′ -6 "	12	#9
>10 - 15	3′-0 "	11′-6 "	12'-0"	12	#9
>15 - 20	3′-0 "	13′-0"	13′-0"	12	#9
>20 - 25	3′-0"	13′ -6 "	14'-0"	12	#9
>25 - 30	3′-0"	14′ -6 "	15′-0"	12	#9
>30 - 35	3′-0"	15′-0"	15′-6"	12	#9
>35 - 40	3′-6 "	15′-6 "	16′ -6 "	14	#9
>40 - 45	3′-6 "	15′-6 "	17′-0"	14	#9
>45 - 50	3′-6 "	16′-6 "	17′-6"	14	#9
>50 - 60	3′-6″	17′-0"	18′-6 "	14	#9

\* TWO ARMS PERPENDICULAR TO EACH OTHER. ADDITIONAL STRUCTURAL ANALYSIS IS REQUIRED FOR TWO MAST ARMS AT ACUTE OR OBTUSE ANGLES TO EACH OTHER.

#### MAST ARM FOUNDATION NOTES:

1. WHEN THE SHAFT OF THE SUPPORT IS EXTENDED IN LENGTH AND PROVIDED WITH A LUMINAIRE ARM, OR WHEN THE SHAFT OF THE SUPPORT IS EXTENDED IN LENGTH BY 36" MINIMUM TO ALLOW FOR INSTALLATION OF A LUMINAIRE IN THE FUTURE VIA AN OVERLAP SLIP JOINT, THE DEPTH "H" REQUIRED BY THE DESIGN TABLE FOR THE TYPE "A" FOUNDATION SHALL BE INCREASED BY 8".

2. NO DEVIATION IN THE FOUNDATION DESIGN GIVEN HERE IS REQUIRED WHEN THE TRAFFIC SIGNAL CONTROLLER CABINET IS MOUNTED ON THE SHAFT.

3. MAST ARM FOUNDATIONS ARE BASED ON STANDARD STRUCTURE LOADINGS SHOWN IN THE DEPARTMENT'S "CRITERIA FOR THE DESIGN OF TRAFFIC SIGNAL SUPPORTS", PUBLICATION 149. FOUNDATION DESIGN ASSUMES :

- LUMINAIRE, WHEN USED, HAS A 30' MOUNTING HEIGHT AND A 15' ARM LENGTH.
   THE CENTROID OF SIGNALS AND SIGNS ON MAST ARM AT 20' MAXIMUM FROM TOP OF THE FOUNDATION.
   A CABINET, WHEN USED, HAS A 51" HEIGHT, 30" WIDTH, 22" DEPTH AND DEAD LOAD OF 281 LBS WITH CENTROID LOCATED AT 54" MAXIMUM FROM TOP OF THE FOUNDATION.
- 4. WHEN A MAST ARM SUPPORT HAS TWO ARMS WHICH ARE PERPENDICULAR TO EACH OTHER, USE THE FOUNDATION IN THE DESIGN TABLE FOR THE LENGTH OF THE LONGER ARM.



			SHAFT LENGTH 20' - 34'										
DESIGN	"D "	"W"	BAR	20' SHAFT	22′ SHAFT	24′ SHAFT	26' SHAFT	28′ SHAFT	30' SHAFT	32' SHAFT	34′ SHAFT		
(LBS)	(FT)	QTY.	SIZE	FOUNDATION DEPTH H (FT)									
1000	3'-0"	12	#9	11'-0"	11′-6"	11′-6 "	12'-0"	12′ -6 "	12′-6″	13′-0"	13′-0"		
2000	3'-0"	12	#9	12′ -6 "	13′-0"	13′ -0 "	13′-6"	14′ -0 "	14′-0"	14′-6 "	14' -6 "		
3000	3′-0"	12	#9	14′ -0 "	14′-0"	14′ -6 "	15′-0"	15′-0"	15′-0"	15′-6″	16′-0″		
4000	3′-0″	12	#9	15'-0"	15′-0"	15′ -6 "	16′-0″	16′-0″	16′-6″	17′-0"	17′-0"		
5000	3′-0″	12	#9	16' - 0 "	16′-0"	16′ -6 "	17′-0"	17′-0"	17-16"	18′-0"	18′-0"		
6000	3′-0″	12	#9	16' - 6 "	17′-0"	17′-0"	17′-6″	18′-0"	18′-0"	18′-6″	19'-0"		
7000	3′-0″	12	#9	17′-6 "	17′-6 "	18′-0 "	18′-6″	19′-0"	19′-0"	19′-6″	20' -6 "		
8000	3′-0″	16	#9	18'-0"	18′ -6 "	19′-0"	19′-6″	19′ -6 "	20' -6 "	21′-0"	21'-6"		
9000	3′-0″	16	#9	19'-0"	19′-0"	19′ -6 "	20' -6 "	21′-0"	21′-6″	22'-0"	22'-6"		
10,000	3′-0"	16	#9	19' - 6 "	20′ -6 "	21′-0"	21′-6″	22'-0"	22′-6″	23' -6 "	24'-0"		

SHAFT LENGTH	"D "	ANCHOR BOLTS			DEDTU	"W" BAR		
(FT)	(FT)	QTY.	DIA. (IN)	LENGTH (FT)	H (FT)	QTY.	SIZE	
0' - 10'	3'-0"	6	3⁄4 "	2'-0"	6′-0"	8	#8	
>10' - 14'	3'-0"	6	3⁄4 "	2'-0"	6'-6"	8	#8	

#### STRAIN POLE FOUNDATION NOTES:

- 1. NO DEVIATION IN THE FOUNDATION DESIGN GIVEN HERE IS REQUIRED WHEN A TRAFFIC SIGNAL CONTROLLER CABINET OF THE FOLLOWING SIZE IS MOUNTED ON THE SHAFT:

LENGTH OF STRAIN POLE (FT)	LUMINAIRE MOUNTING HEIGH "X" (FT)
20', 22', AND 24'	30′
26′, 28′, AND 30′	35'
32' AND 34'	40'

CLOSED TIE DETAIL

PLAN

#### FOUNDATION FOR TRAFFIC SIGNAL SUPPORT, STRAIN POLE

#### FOUNDATION FOR TRAFFIC SIGNAL SUPPORT, PEDESTAL DESIGN TABLE

MAXIMUM CABINET SIZE: 51" HEIGHT, 30" WIDTH, AND 22" DEPTH WITH DEAD LOAD OF 281 LBS AND CENTROID HEIGHT LOCATED AT 54" MAXIMUM FROM TOP OF THE FOUNDATION.

2. NO DEVIATION IN THE FOUNDATION DESIGN GIVEN HERE IS REQUIRED WHEN THE SHAFT OF THE SUPPORT IS EXTENDED IN LENGTH AND PROVIDED WITH A LUMINAIRE ARM, OR WHEN THE SHAFT OF THE SUPPORT IS EXTENDED IN LENGTH BY 36" MINIMUM TO ALLOW FOR INSTALLATION OF A LUMINAIRE IN THE FUTURE VIA AN OVERLAP SLIP JOINT. THE FOUNDATION DESIGN ASSUMES A 15' LUMINAIRE ARM LENGTH AND THE FOLLOWING LUMINAIRE MOUNTING HEIGHTS:

Г	

"W" BAR

#5 BAR

#### NOTES:

- PROVIDE THE TYPE "A" FOUNDATION AT ALL LOCATIONS, EXCEPT THE TYPE "B" FOUNDATION (SHOWN ON SHEET 5) MAY BE USED WHEN PHYSICAL CONDITIONS PREVENT PLACING THE TYPE "A" FOUNDATION TO ITS REQUIRED DEPTH.
- 2. FOR DESIGN CRITERIA SEE SHEET 3.
- 3. IN A PAYED AREA, PLACE THE TOP OF FOUNDATION FLUSH WITH THE SURFACE OF THE ADJACENT PAVEMENT. IN UNPAVED AREAS TOP OF FOUNDATION TO BE AT LEAST 6" ABOVE TOP OF GROUND.
- 4. FOR GROUND ROD SIZE AND INSTALLATION DETAILS, SEE TC-8804.
- 5. IN A PAVED AREA, GROUT SHALL BE PLACED.

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DEPARTMENT	OF	TRA	NSPOR	RTAT	ION
BUREAU OF HIGHWAY	SAFET	Y AND	TRAFFIC	ENGINE	ERING

#### STANDARD

#### TRAFFIC SIGNAL SUPPORT

#### FOUNDATION TYPE A

	-	
RECOMMENDED Oct.14,2010	RECOMMENDED Oct.14,2010	SHEET 4 OF 7
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#### FOUNDATION FOR TRAFFIC SIGNAL SUPPORT, MAST ARM

MAST ARM	"D "	"W "	BAR	"L " BAR	Y	S	(FT)	7	S	(FT)
(FT)	(FT)	QTY.	SIZE	SIZE	(FT)	ONE ARM	TWO ARMS*	( FT)	ONE ARM	T₩O ARMS*
0 - 10	3′-0"	12	#9	#4	4′-0"	9′-6″	9′-6″	5'-0"	9′ - 6 "	9′-6″
>10 - 15	3'-0"	12	#9	#4	4' - 0 "	10′ -6 "	10′ -6 "	5'-0"	10' -6 "	10' -6 "
>15 - 20	3′-0"	12	#9	#5	4′-0"	11′-6 "	11' -6 "	5′-6″	11'-6"	11'-6"
>20 - 25	3′-0"	12	#9	#6	4′-0"	12'-0"	12'-0"	6′-0"	12'-0"	12'-0"
>25 - 30	3'-0"	12	#9	#6	4′-6 "	12' -6 "	13′-0"	6' - 6 "	12' -6 "	12' -6 "
>30 - 35	3'-0"	12	#9	#7	4′-6 "	13′-0"	13′ -6 "	7′-0"	13'-0"	13'-6"
>35 - 40	3'-6"	14	#9	#7	5'-0"	13′-6"	14'-0"	7′-0"	13'-0"	13'-6"
>40 - 45	3'-6"	14	#9	#7	5'-0"	13′-6"	14' -6 "	7′-6″	13'-0"	13'-6"
>45 - 50	3'-6"	14	#9	#7	5'-6"	14′-0"	14' -6 "	8′-0"	13'-0"	13'-6"
>50 - 60	3'-6"	14	#9	#8	5'-6"	14'-6"	16'-0"	8'-0"	13'-6"	14' -6 "

\* TWO ARMS PERPENDICULAR TO EACH OTHER. ADDITIONAL STRUCTURAL ANALYSIS IS REQUIRED FOR TWO MAST ARMS AT ACUTE OR OBTUSE ANGLES TO EACH OTHER.

#### MAST ARM FOUNDATION NOTES:

- 1. NO DEVIATION IN THE FOUNDATION DESIGN GIVEN HERE IS REQUIRED WHEN THE SHAFT OF THE SUPPORT IS EXTENDED IN LENGTH AND PROVIDED WITH A LUMINAIRE ARM, OR WHEN THE SHAFT OF THE SUPPORT IS EXTENDED IN LENGTH BY 36" MINIMUM TO ALLOW FOR INSTALLATION OF A LUMINAIRE IN THE FUTURE VIA AN OVERLAP SLIP JOINT. THE FOUNDATION DESIGN ASSUMES A 15' LUMINAIRE ARM LENGTH AND A 30' MOUNTING HEIGHT.
- 2. NO DEVIATION IN THE FOUNDATION DESIGN GIVEN HERE IS REQUIRED WHEN A TRAFFIC SIGNAL CONTROLLER CABINET OF SIZE SPECIFIED ON SHEET 4 IS MOUNTED ON THE SHAFT.

3. MAST ARM FOUNDATIONS ARE BASED ON STANDARD STRUCTURE LOADINGS SHOWN IN THE DEPARTMENT'S "CRITERIA FOR THE DESIGN OF TRAFFIC SIGNAL SUPPORTS", PUBLICATION 149. FOUNDATION DESIGN ASSUMES THAT THE CENTROID OF SIGNALS AND SIGNS ON MAST ARM AT 20' MAXIMUM FROM TOP OF THE FOUNDATION.

4. WHEN A MAST ARM SUPPORT HAS TWO ARMS WHICH ARE PERPENDICULAR TO EACH OTHER, USE THE FOUNDATION IN THE DESIGN TABLE FOR THE LENGTH OF THE LONGER ARM.

#### NOTES:

- 1. THE TYPE "B" FOUNDATION MAY BE AUTHORIZED FOR USE WHERE CONDITIONS PREVENT PLACING THE TYPE "A" FOUNDATION (AS SHOWN ON SHEET 4 ) TO ITS REQUIRED DEPTH.
- 2. FOR DESIGN CRITERIA SEE SHEET 3.
- 3. IN A PAVED AREA, PLACE THE TOP OF FOUNDATION FLUSH WITH THE SURFACE OF THE ADJACENT PAVEMENT. IN UNPAVED AREAS TOP OF FOUNDATION TO BE AT LEAST 6" ABOVE TOP OF GROUND.

DESIGN

(LBS)

- FOR GROUND ROD SIZE AND INSTALLATION DETAILS, SEE TC-8804.
- DISTANCE "F" AS REQUIRED TO AVOID PAVEMENT AND/OR CURB EXCAVATION.
- 6. SEE SHEET 4 FOR CLOSED TIE DETAIL.
- 7. IN A PAVED AREA, GROUT SHALL BE PLACED.



<u>SECTION G-G</u>

(FOR CLARITY, CONDUIT IS NOT SHOWN)

SHAFT LENGTH 20' - 24' SHAFT LENGTH 26' - 30' "W" BAR "W" BAR BAR BĂR TENSION "D " "D" (FT) (ĔT) ( FT) (FT) (ĔT) (FT) (FT) (FT) (FT) (FT)  $(\dot{ET})$ QTY. SIZE SIZE QTY. SIZE SIZE 1000 3′-0″ 12 #9 #4 4′-0″ 9′-6″ 9′-0″ 4′-0″ 9′-6″ 9′-0″ 3′-0″ 12 #9 #4 4′-0″ 10′-6″ 10′-6″ 4′ 

 2000
 3'-0"
 12
 #9
 #4
 4'-0"
 10'-6"
 10'-6"
 10'-6"
 3'-0"
 12
 #9
 #5
 4'-0"
 12'-0"
 4'

 3000
 3'-0"
 12
 #9
 #5
 4'-0"
 11'-6"
 10'-6"
 3'-0"
 12
 #9
 #5
 4'-0"
 12'-0"
 4'

 3000
 3'-0"
 12
 #9
 #5
 4'-0"
 13'-0"
 5'

 4000 3′-0" 12 #9 #5 4′-0" 12′-0" 12′-0" 5′-0" 12′-0" 12′-0" 12′-0" 12′-0" 12′-0" 12′-0 4″ 3′-0" 12 #9 #6 4′-6" 14′-0" 14′-0" 6′ 5000 3'-0" 12 #9 #6 4'-6" 13'-0" 12'-6" 6'-0" 12'-6" 3'-0" 12 #9 #6 5'-0" 14'-6" 14'-6" 6' 6000 3′-0" 12 **#9 #6** 5′-0" 13′-0" 13′-0" 6′-6" 12′-6" 12′-6" 12′-6" 12′-6" 12′-6" 12′-6" 7′ 7000 3′-0″ 12 #9 #7 5′-0″ 13′-6″ 13′-6″ 13′-6″ 13′-0″ 13′-0″ 13′-0″ 13′-0″ 12 #9 #7 6′-0″ 15′-0″ 15′-0″ 8′ 8000 3'-0" 12 #9 #7 5'-6" 14'-0" 14'-0" 7'-6" 13'-0" 13'-0" 3'-0" 12 #9 #8 6'-6" 15'-6" 15'-6" 8'

9000 3′-0" 12 #9 #7 6′-0" 14′-0" 14′-0" 8′-0" 13′-6" 13′-6" 3′-0" 16 #9 #8 7′-0" 15′-6" 15′-6" 9′ 10,000 3′-0″ 12 #9 #8 6′-6″ 14′-6″ 14′-0″ 8′-6″ 13′-6″ 13′-6″ 3′-0″ 16 #9 #9 7′-6″ 15′-6″ 15′-6″ 10′

S<sup>L</sup> = WITH LUMINAIRE



TYPE B FOUNDATION

#### FOUNDATION FOR TRAFFIC SIGNAL SUPPORT, STRAIN POLE

				SHAFT LENGTH 32' - 34'									
Z E T)	S <sup>L</sup>	S (ET)	"D"	"W" BAR		"L " BAR	Y (ET)	S <sup>L</sup>	(ET)	Z	S <sup>L</sup>	S (ET)	
,		(11)	(117	QTY.	SIZE	SIZE	(11)	(11)	(11)	(11)	(11)		
- 0 ''	10′ -6 "	10' -0"	3′-0"	12	#9	#4	4' - 0 "	11'-0"	10′ -6 "	4′-0"	11'-0"	10′-6"	
- 0 "	12' -0 "	11'-6"	3'-0"	12	#9	#5	4'-0"	12' -6 "	12'-0"	4′-0"	12' -6 "	12'-0"	
- 0 "	12' -6 "	12'-0"	3'-0"	12	#9	#6	4'-0"	13′-6"	13' - 0 "	5′-0"	12' -6 "	12'-6"	
- 0 "	12' -6 "	12' -6 "	3'-0"	12	#9	#6	4' - 6 "	14' -0"	14' -0 "	6′-0"	13' - 0 "	13′-0"	
-6"	13' - 0 "	13' - 0 "	3'-0"	12	#9	#7	5'-0"	14' -6 "	14' -6 "	6' - 6 "	13' -6 "	13′-0"	
- 0 "	13′ - 6 "	13' - 0 "	3'-0"	12	#9	#7	5'-6"	14' -6 "	14' -6 "	7′-0"	14' -0 "	13′-6"	
- 0 "	13′ - 6 "	13′ - 6 "	3'-0"	16	#9	#8	6'-0"	15'-0"	15'-0"	8′-0"	14' -0 "	13′-6"	
-6"	13′ - 6 "	13′-6"	3'-0"	16	#9	#8	6'-6"	15′-6"	15′-6"	8′-6 "	14' -0 "	14′-0"	
- 0 ''	14' -0 "	13' -6 "	3'-0"	16	<b>#</b> 9	#9	7′-0"	15'-6"	15'-6"	9′-0"	14' -6 "	14' -6 "	
- 0 "	14' -0 "	14' -0"	3'-0"	16	<b>#</b> 9	#9	7′-6"	15'-6"	15'-6"	10' -0"	14' -6 "	14'-6"	

#### STRAIN POLE FOUNDATION NOTES:

- NO DEVIATION IN THE FOUNDATION DESIGN GIVEN HERE IS REQUIRED WHEN A TRAFFIC SIGNAL CONTROLLER CABINET OF SIZE SPECIFIED ON SHEET 4 IS MOUNTED ON THE SHAFT.
- 2. USE S FOUNDATION SIZE WHEN THE SHAFT OF THE SUPPORT IS EXTENDED IN LENGTH AND PROVIDED WITH A LUMINAIRE ARM, OR WHEN THE SHAFT OF THE SUPPORT IS EXTENDED IN LENGTH BY 36" MINIMUM TO ALLOW FOR INSTALLATION OF A LUMINAIRE IN THE FUTURE VIA AN OVERLAP SLIP JOINT. THE FOUNDATION DESIGN ASSUMES A 15' LUMINAIRE ARM LENGTH AND THE FOLLOWING LUMINAIRE MOUNTING HEIGHTS:

LENGTH OF STRAIN POLE (FT)	LUMINAIRE MOUNTING HEIGHT "X" (FT)
20', 22', AND 24'	30′
26′, 28′ AND 30′	35′
32' AND 34'	40′

\*\* DIAMETER IF CIRCULAR, OR SIDE IF SQUARE. CIRCULAR FOUNDATIONS SHALL BE SQUARE FROM THE TOP TO A POINT G" BELOW THE GROUND LINE, IF SIDEWALK IS PRESENT.





#### TRAFFIC SIGNAL SUPPORT

## FOUNDATION TYPE B











NOTE: BASE-I	MOUNTED CONTROLLER ASSEMBLIES	
LOCAT HAVE CABIN	ED IN A PAVED SURFACE SHALL THE ANCHOR BOLTS INSIDE THE ET.	
DED		
.)	0.75" M1" DIA DRAIN	
.)		
	ANCHOR BOLT (SEE NOTE 6)	
	(SEE NOTES 1 AND 7)	
PAVED	SURFACE	
	COMMONWEALTH OF PENNSYL	VANIA
	BUREAU OF HIGHWAY SAFETY AND TRAFFIC ENGL	NEERING
	STANDARD	
	CONTROLLED ACCEMPLY	
	CONTROLLER ASSEMBLT	
	RECOMMENDED Oct.14,2010 RECOMMENDED Oct.14,2010	SHT. 1 OF 1
	CHIEF, TRANSPORTATION OPERATIONS DIVISION ACTIVE SAFETY AND TRAFFIC ENGINEERING	TC-8802



#### NOTES:

- 1. PROVIDE 24" MINIMUM CLEARANCE. IF THERE IS NO CURB, CLEARANCE IS FROM EDGE OF SHOULDER.
- 2. FOR DETAIL OF FOUNDATION, SEE TC-8801.
- 3. PROVIDE 3"  $\times$  5" HANDHOLE OPENING WITH A MINIMUM FRAME THICKNESS OF  $\frac{3}{3}$  ".
- 4. DIMENSIONS "M" AND "N" ARE FROM SIDEWALK. IF NO SIDEWALK, DIMENSIONS ARE FROM PAVEMENT GRADE AT CENTER OF ROADWAY. PROVIDE SPECIFIED DIMENSION "M" SUCH THAT CLEARANCE IS IN THE RANGE OF 8' MINIMUM, 19' MAXIMUM FOR TRAFFIC SIGNAL HEADS. PROVIDE SPECIFIED DIMENSION "N" SUCH THAT CLEARANCE IS IN THE RANGE OF 7' MINIMUM, 10' MAXIMUM FOR PEDESTRIAN SIGNAL HEADS.
- 5. IN A PAVED AREA, PLACE THE TOP OF THE FOUNDATION FLUSH WITH THE SURFACE OF THE ADJACENT PAVEMENT.
- 6. ALL ACCESSIBILITY FEATURES MUST BE COMPLIANT TO PENNDOT PUB-LICATION 13M (DM-2), CHAPTER 6, PUBLICATION 72M (RC STANDARDS) CRITERIA AND PUBLICATION 149.
- PEDESTRIAN PUSHBUTTONS SHALL BE OF A TYPE APPROVED BY THE DEPARTMENT AND LISTED IN PUBLICATION 35 (BULLITIN 15).
   PEDESTRIAN PUSHBUTTONS SHOULD BE A MINIMUM OF 2" DIAMETER AND A FORCE PER ACTUATION THAT CANNOT EXCEED 5 LBS.
- 9. PROVIDE 4'-0"  $\times$  4'-0" MINIMUM LANDING WITH 2.00% MAXIMUM SLOPE IN ALL DIRECTIONS WHERE PEDESTRIANS PERFORM 180° TURNING MANEUVERS.



STANDARD

MISCELLANEOUS TRAFFIC SIGNAL SUPPORT-PEDESTAL PEDESTRIAN PUSHBUTTON

RECOMMENDED Oct.14,2010	RECOMMENDED <u>Oct.14,2010</u>	SHT. 1 OF 2
CHIEF, TRANSPORTATION OPERATIONS DIVISION	ACTING DIR. BUR. OF HIGHWAY SAFETY AND TRAFFIC ENGINEERING	TC-8803





ETER SOCKE ETER (IF F	ET AND REQUIRED)
"Ø CONDUI" ERVICE DIS SEE TYPICA	T (MIN.) SCONNECT AL WIRING
IAGRAM ) - 2 "Ø COND (MIN.) N	
	IF END OF CABINET WILL NOT ACCOMMODATE BASE-MOUNTED METER SOCKET AND CONTROLLER SERVICE DISCONNECT,
	ASSEMBLY LETHER ONE OR BOTH MAY BE PLACED ON THE BACK OF THE CABINET.
· · · ·	
	24" (MIN.)
SERV FROM UT	
	FRONT VIEW 2"Ø CONDUIT
ND ROD (SE ECT TO GRO ERVICE DIS NDING BUS	RVICE), (MIN.) JUNDING BUS SCONNECT AND IN CONTROLLER
NET WITH # ND WIRE. ERVICE	*4 AWG (MIN.) TYPE C
BARE STRAN ER GROUND (TYP.)	ADED SERVICE DISCONNECT SERVICE WIRE (TYP.)
	GROUND ROD 5% "Ø (MIN.)
-	10' (MIN.) 10' (MIN.) 10' (MIN.)
	SERVICE GROUNDING ELECTRODE SYSTEM
	NOTE:
	<ol> <li>FOR DETAIL OF TRAFFIC SIGNAL SUPPORT FOUNDATION, SEE TC-8801.</li> <li>FOR DETAIL OF CONTROLLER ASSEMBLY FOUNDATION, SEE TC-8802.</li> </ol>
	<ol> <li>ALL GROUND RODS ARE 5/2 " DIA. (MIN.) × 10' LONG (MIN.). USE EXOTHERMIC WELD OR BRONZE CONNECTOR TO CONNECT GROUND WIRE TO GROUND ROD.</li> </ol>
	<ol> <li>INSTALL SERVICE TYPES A, B OR C AS APPROVED BY THE UTILITY COMPANY.</li> </ol>
	<ol> <li>PROVIDE ALL SERVICE CONDUITS OF THE HDG RIGID METALLIC TYPE WITH WATERTIGHT CONDUIT HUBS.</li> </ol>
	<ol> <li>REFER TO UTILITY'S SERVICE DETAIL WHEN UNMETERED LIGHTING IS INSTALLED ON TRAFFIC POLES. A SEPARATE DISCONNECT MAY BE REQUIRED.</li> </ol>
	<ol> <li>PROVIDE THE SERVICE DISCONNECT INSIDE AN OPTIONAL ALUMINUM ENCLOSURE, WHERE INDICATED.</li> </ol>
	8. PROVIDE ADDITIONAL BREAKERS AS REQUIRED FOR LIGHTING LOADS.
	COMMONWEALTH OF PENNSYLVANIA
	DEPARTMENT OF TRANSPORTATION BUREAU OF HIGHWAY SAFETY AND TRAFFIC ENGINEERING
	STANDARD
	FLECTRICAL DISTRIBUTION
OUNDING M	
	RECOMMENDED <u>oct.14,2010</u> Close RECOMMENDED <u>oct.14,2010</u> SHT. 1 OF 2 SHT. 1 OF 2 SHT. 1 OF 2
	CHIEF, TRANSPORTATION OPERATIONS ACTING DIR. BUR. OF HIGHWAY   IC-8804



ACKFILL. MATERIAL IN	TO BOTTOM OF EXISTING SUBBASE. BACKFILL AS SPECIFIED IN SECTION 954, PUBLICATION 408 REPLACE SUBBASE IN KIND. REPLACE IN KIND.	•
СН А	ND BACKFILL	
	AND A MINIMUM OF TWO CORROSION RESISTANT FASTENERS.	
	<ol> <li>JUNCTION BOXES USE JB-26 AND JB-27 ONLY IN AREAS NOT SUBJECT TO VEHICULAR TRAFFIC.</li> </ol>	
	<ol> <li>JUNCTION BOXES BOTTOM MAY BE OPEN OR CLOSED. IF CLOS PROVIDE A DRAIN HOLE 2" DIAMETER MINIMUM.</li> </ol>	SED,
	4. FOR DETAIL OF JUNCTION BOXES JB-1, JB-2, JB-11 AND JB-1: SEE STANDARD DRAWINGS, RC-81M AND RC-82M OF PENNDOT PUB	2, . 72M.
	<ol> <li>GROUND EXPOSED METAL PARTS OF JUNCTION BOXES. USE GROU LUGS. DO NOT CONNECT GROUND WIRE DIRECTLY TO LID.</li> </ol>	NDING
	COMMONWEALTH OF PENNSYLVAN	[A
	DEPARTMENT OF TRANSPORTATION bureau of highway safety and traffic engineering	
	STANDARD	
	ELECTRICAL DISTRIBUTION	
<u>) X</u>		
	RECOMMENDED UCC. 14, 2010 RECOMMENDED UCC. 14, 2010 SHT. 2 SHT. 2 SHT. 2	
	CHIEF, INANSPORTATION OPERATIONS ACTING DIR "BUR. OF HIGHWAY DIVISION SAFETY AND TRAFFIC ENGINEERING	3804







D	ETECTORS	
RECOMMENDED Oct.14,2010	RECOMMENDED	SHT. 2 OF 2
CHIEF, TRANSPORTATION OPERATIONS DIVISION	ACTING DIR. BUR. OF HIGHWAY SAFETY AND TRAFFIC ENGINEERING	TC-8806

COMMONWEALTH OF PENNSYLVANIA

DEPARTMENT OF TRANSPORTATION

BUREAU OF HIGHWAY SAFETY AND TRAFFIC ENGINEERING

STANDARD

ALTERNATE C SPLICE WILL BE MADE ELECTRICALLY SECURE WITH INSULATED COMPRESSION CONNECTORS THEN COVERED WITH A SPLICING KIT THAT IS WOISTURE-PROOF, SPLICE ENCAPSULATING (INCLUDING CABLE JACKET), AND DESIGNED FOR INSULATING AND SPLICING ELECTRIC CABLE; OR A RE-ENTERABLE SPLICE KIT AS SPECIFIED IN SEC. 1104.07(g)4, PUBLICATION 408.

ALTERNATE C

## 20.0 CRITERIA FOR THE DESIGN OF TRAFFIC SIGNAL SUPPORTS

The criteria stated herein shall be utilized in the design of galvanized steel structures used for the support of traffic signals.

## 20.1 PART A - DESIGN CRITERIA FOR ALL SUPPORT STRUCTURES

(See Section 20.2; Part B, "Design Criteria for Strain Poles," for additional requirements for strain poles.)

Vertical poles and mast arms shall be designed and constructed in accordance with the 2001 AASHTO "Standard Specifications for Structural Supports for Highway Signs, Luminaires and Traffic Signals" including interim specifications (2002, 2003, and 2006), hereafter referred to as the "AASHTO Specifications." In this part, the AASHTO Specifications article numbering system is followed. Where new sections, articles, equations, figures, or tables have been added, the suffix P is used to designate "Pennsylvania Article." All references to the AASHTO Specifications sections, articles, equations, figures, or tables carry the prefix A, except where noted. References to the AASHTO Specifications commentary carry the prefix AC, except where noted.

- Provide base and connection plates as indicated in Publication 148; TC-8801 sheet 7 of 7.
- Provide a complete joint penetration weld for the connection of the column or shaft to the base plate and the connection of the arm to the flange plate for mast arm and strain pole structures only (this is not a requirement for pedestal poles).
- Attach a back-up ring as specified in the AASHTO Specifications (Table 11-2, Detail 11). The backing ring shall be attached to the plate with a full-penetration weld or with a continuous fillet weld around the interior face of the backing ring.
- For pole diameters 18 inch and larger, seal the top of the backing ring with a continuous 1/8 inch fillet weld to seal off the area between the ring and the pole. For pole diameters less than 18 inch, seal the top of the backing ring with a continuous bead of caulk after galvanizing to seal off the area between the ring and the pole.
- Provide 6 inch complete penetration longitudinal shaft welds at the base plate connection.
- The use of mast arm plate socket connections with fillet welds are prohibited.
- Provide welded connections as shown in Publication 148; TC-8801 sheet 7 of 7.
- The minimum thickness for column and mast materials shall be 3/16 inch or 7 gauges. A non-destructive testing plan is required to be submitted to the

Bureau of Construction Materials for materials less than 5/16 inch.

• Provide a built-up box on columns with mating splice plate for mast arm connection as shown in Example 8 of Figure 11-1(c) in AASHTO Specifications. With prior Department approval, alternate mast arm connections as shown in the AASHTO Specifications (Example 16 of Figure 11-1(c)) are permitted.

## Section 1: Introduction

## Section 1.3 APPLICABLE SPECIFICATIONS

The following shall replace the first sentence of A1.3.

The following specification documents shall be referenced for additional information on design, materials, fabrication, and construction:

The following shall supplement A1.3.

e) PENNDOT Publication 408.

## Section 2: General Features of Design

#### 2.5 ROADSIDE REQUIREMENTS FOR STRUCTURAL SUPPORTS

#### 2.5.2 Breakaway Supports

The following shall supplement A2.5.2.

Breakaway supports or yielding-type supports shall not be used for traffic signal support structures, except when permitted by this Handbook and specified in the plans and/or specifications for the project.

## Section 3: Loads

## 3.5 DEAD LOAD

The following shall supplement A3.5.

Dead loads for signs, traffic signals, backplates, brackets, and all appurtenances shall be as given in this Handbook.

## 3.6 LIVE LOAD

Delete A3.6.

## 3.8 WIND LOAD

The following shall replace A3.8.

Wind load shall be the pressure of the wind acting horizontally on the supports, signs, luminaires, traffic signals, and other attachments computed in accordance with this Handbook and AASHTO Appendix C.

## Section 5: Steel Design

## **5.14 DETAILS OF DESIGN**

## **5.14.3 Slip Type Field Splice**

The following shall replace A5.14.3.

Telescoping (slip-fit) splices for mast arms, which rely solely on friction between the members for their connection, will not be permitted. A thru-bolt must be provided for a positive connection when such slip fit connections are used.

## 5.15 WELDED CONNECTIONS

The following shall supplement A5.15.

Transverse welds shall not be used to splice pole sections.

## **5.17 ANCHOR BOLTS**

#### 5.17.3 Design Basis

The following shall supplement A5.17.3.

A minimum of six (6) anchor bolts shall be required.

#### 5.17.6.4 Bending Stress in Anchor Bolts

The following shall replace A5.17.6.4.

The clearance between the bottom of the leveling nuts and the top of the concrete foundation shall not be greater than one bolt diameter.

## 5.18 MINIMUM PROTECTION FOR STRUCTURAL STEEL

## 5.18.1 General

The following shall replace the first sentence of A5.18.1.

Steel structures shall be protected from the effects of corrosion including those manufactured of high strength steel, by means of galvanizing in accordance with ASTM A 123 (AASHTO M 111). Accessories and hardware shall also be protected from the effects of corrosion by means of galvanizing in accordance with ASTM A 153 (AASHTO M 232).

## Section 11: Fatigue Design

## **11.6 FATIGUE IMPORTANCE FACTORS**

The following shall supplement A11.6.

Traffic signal structures with mast arms less than or equal to 60 feet shall be designed for Fatigue Category II. Traffic signal structures with mast arms greater than 60 feet shall be designed for Fatigue Category I. Strain poles should be considered as an alternative to traffic signal structures with mast arms greater than 60 feet.

#### **11.7 FATIGUE DESIGN LOADS**

#### 11.7.1 Galloping

The following shall replace A11.7.1.

The dead load and wind surface area of a standard mitigation device shall be considered in the design of cantilevered traffic signal support structures in accordance with the standard drawings. The mitigation device should be installed only within the 180-day monitoring period in accordance with the standard drawings.

#### 11.7.4 Truck-Induced Gust

Delete A11.7.4.

## Section 14P: Design Aids

This section shall supplement AASHTO Appendix B.

#### **14.2P STRESSES FOR TUBULAR SECTIONS**

The following shall supplement Table 20-2:

Maximum shear stress due to torsion  $(f_{vt})$  for round stepped tubes (hot-swaged shrink fit) shall be computed using the following formula:

$$f_{vt} = \frac{M_z k_t}{6.28R^2 t}$$

Where:

 $f_{vt}$  = Maximum shear stress due to torsion,  $lb/in^2$ 

 $M_z$  \_ Total torsional moment, in-lb

R = Radius at mid-thickness of smaller diameter tube wall, in

t = Thickness of smaller diameter tube wall, in

 $k_t$  = Stress concentration factor due to change in tube diameter (use  $k_t = 1.20$ )

## Section 15P: Alternate Method for Wind Pressures

This section shall supplement AASHTO Appendix C.

#### **15.2P WIND LOAD**

The following shall replace the second sentence of the first paragraph of C.2:

The design wind pressures shall be computed using the wind pressure formula, Eq. C-1, for a fastest-mile wind speed ( $V_{fm}$ ) of 80 MPH as shown in Figure C-3.

## 20.2 PART B - DESIGN CRITERIA FOR STRAIN POLES

(See Section 20.1; Part A, "Design Criteria for All Support Structures," for additional requirements.)

## 1. Allowable Unit Stresses

The design and construction of strain pole structures shall conform to the allowable unit stresses provided in Section 5 – Steel Design in the 2001 AASHTO "Standard Specifications for Structural Supports for Highway Signs, Luminaires and Traffic Signals", hereafter referred to as the "AASHTO specifications."

#### 2. Span and Tether Wires

Span wire shall conform to ASTM A 475, Class A, Siemens-Martin Grade, or ASTM B 416. Tether wire shall conform to ASTM A 475, Class A, Common Grade.

Strain poles shall be designed for a sag of 5% of the span distance between poles under dead load. In computing dead load, the mass of the span and tether wire shall be based on a value of 1 lb/ft [load=1 lb/ft].

#### 3. Strain Pole Deflection

The maximum horizontal deflection of strain poles, at the span wire connection, due to dead loads only, shall be 2.5% of the distance measured from the base of the strain pole to the span wire connection point.

When strain poles support more than one span, the resultant horizontal deflection, due to the combined action of all span wire loadings, shall not exceed the above.

#### 4. Stringing Tension

To determine the stringing tension in the span wire system between the two strain poles, due to the dead loads of traffic signals, traffic signs, signal wire, and other attachments, the following procedure<sup>1</sup> shall be used:

- a. Determine the effective load of each item on the span wire (traffic signal, traffic sign, signal wire, and/or other attachment) by adding to the load of each item, the load of the span wire for a length equal to half the distance in each direction to the next adjacent item or strain pole.
- b. Determine the vertical reaction at each strain pole structure by summing the moments (due to the effective load of each item and the vertical reaction at the strain pole) about the other strain pole structure. As a check, the sum of the vertical reactions of the two strain pole structures should be equivalent to the sum of the effective loads of each item.
- c. Determine the lowest point due to sag in the span wire by finding the point at which the slope of the span wire changes sign (which will be at the location of one of the load items, most probably a traffic signal). Beginning with the vertical reaction at one of the strain pole structures, determine the vertical shear acting on the span wire by successively and algebraically adding the effective load of each item in moving across to, and ending with the vertical reaction of, the other strain pole structure. The low point in the span wire is the point at which the sign of the vertical shear changes (which indicates that the slope of the span wire has changed). If the vertical shear happens to be zero at any point between the strain pole structures, this indicates that two load items are at the same elevation and share the low point of the span wire. As a check, the vertical shear must begin and end at zero at the constituent strain pole structures.

<sup>&</sup>lt;sup>1</sup> Based on the General Cable Theorem

- d. Determine the stringing tension by evaluating the summation of moments about the low point in the span wire. Since the span wire cannot resist bending moment, set the sum of the moments about the low point of all forces acting on the span wire between the low point and either of the strain pole structures equal to zero, where the horizontal pull acting on that strain pole structure is an unknown force acting at a distance equal to the maximum allowable sag (5% of the span distance) above the low point of the span wire. The stringing tension in the span wire can then be determined by solving the aforementioned summation for the unknown horizontal force acting on each of the strain pole structures.
- e. In the case where a strain pole structure supports wires and loading from more than one span, determine the stringing tension of each span wire that it supports, and combine these separate stringing tensions to produce the maximum resultant stringing tension acting on the given strain pole structure to evaluate the required design and construction considerations.

#### 5. Sag

To determine the sag at any load item on the span wire, assume that the span wire follows a straight line between adjacent load items which slopes at a rate equal to the vertical shear at the given load item divided by the horizontal stringing tension. The change in elevation between successive load items is then equivalent to the slope of the span wire between these two load items multiplied by the distance between them. As a check, the elevation of the span wire connection at the second strain pole structure must be obtained by beginning with the connection at the first strain pole structure and successively adding the respective elevation increments in moving across the span wire.

#### 6. Application of Wind Load (see Figure B-1)

 $W_h$  for strain pole structures may be applied as a series of concentrated loads along the span wire normal to the span, and  $W_p$  (normal to sign faces) shall be applied normal to the span. Strain poles (assuming a single span wire is attached to the support) shall be designed for wind loads  $W_h$  and  $W_p$ , (normal to the sign faces) applied normal to the span. Only the wind load,  $W_v$ , shall account for wind from any direction. The basic load, BL (see Section 3.9.3 of the AASHTO specifications) normal to the span shall be the effect from the wind load  $W_v$ , applied at the center of pressure of the support. The full transverse component shall be applied to the support.

## 7. Design Tension

For a strain pole structure with the ends of the span wire at the same elevation, the following approximate method may be used to determine the force component in the span wire parallel to the span for a wind loading normal to the span.

The span wire loadings (dead load, wind, and ice) are applied as a series of concentrated loads along the wire to represent the actual uniform loadings with a minimum of five equal concentrated loads recommended. The tension forces throughout the wire now become a series of vectors with the vector component in the direction of the span of equal magnitude for each vector. Knowing that the ratio of the vector length over the vector force is proportional to the ratio of the vector component length over a component force, the length of each vector may be expressed by the following equation:

Vector Length = 
$$\sqrt{\left(F_x^2 + F_y^2 + F_z^2\right)} \frac{d_x}{F_x}$$

Where :

$\sqrt{\left(F_{\rm x}^2\right)}$	$+F_y^2$	$(+F_z^2)$ = Resultant vector force
$F_x$	=	Vector force component in direction of span
$F_y$	=	Vector force component in vertical direction
$F_z$	=	Vector force component in direction of wind
$d_x$	=	Vector length component in direction of span*

(\* If sag is small in relation to span length, neglect any displacements in direction of span.)

 $F_y$  and  $F_z$  for each vector (between concentrated loads of wire, signals, signs, etc.) may be found by the equations of equilibrium for a body in space. The total length of the span wire may be found for a given sag for a loading of dead load alone. The sum of all the vector lengths is equated to the total length of the span wire.  $F_x$  may be solved for since it is the only unknown in the equation. A number of trials may be necessary to closely approximate the actual value.

The following illustrates a procedure for determining the vector components  $F_x$  and  $F_z$ :

In Figure B-2:

 $F_{Z1} = R_{Z(L)}$   $F_{Z2} = R_{Z(L)} - W_A$   $F_{Z3} = R_{Z(L)} - W_A - W_B$   $F_{Z4} = R_{Z(R)} - W_E - W_D$   $F_{Z5} = R_{Z(R)} - W_E$   $F_{Z6} = R_{Z(R)}$ 

The total length of span wire =  $\sqrt{(F_x^2 + F_{y1}^2 + F_{z1}^2)} \frac{d_{x1}}{F_x} + \sqrt{(F_x^2 + F_{y2}^2 + F_{z2}^2)} \frac{d_{x2}}{F_x} + \cdots$ 

The reactions  $R_{z(L)}$  and  $R_{z(R)}$  may be determined by summing moments about a vertical line at the right end and left end of the span wire respectively. A similar procedure is used in determining  $F_y$  components. The reactions in the vertical direction ( $R_{y(L)}$  and  $R_{y(R)}$ ) may be determined by summing moments about a horizontal line to the ends of the span wire.

The above procedure neglects the effect of the strain pole deflection. This results in excessively conservative values for the wire's force component in the direction of the span ( $F_x$ ). The effects of the strain pole deflections on the span wire's force component should be considered by calculating the deflections of the strain pole at the span wire connection, in the direction of the span, and recomputing the wire's force component, as above, after making adjustments to the span to account for the strain pole deflections. The reduction in tension does not apply to dead load tension. Given the wire is installed with the specified sag after the pole dead load deflection already has occurred, the wire tension is not reduced.

#### 8. Design Stresses

Strain pole structures shall be designed and constructed to withstand maximum stresses based on Group I, Group II, and Group III loadings (whichever controls), as defined in the AASHTO specifications. In the case of strain poles which support more than one span, the resultant of the respective tensions for each span shall be used in combination with the wind applied in the direction which produces maximum stress.

## 20.3 PART C - ACCEPTANCE OF STRUCTURAL DESIGNS

The manufacturer shall submit design calculations and detailed structural drawings for those signal supports that are proposed to be supplied in Pennsylvania. In addition, the manufacturer must provide PennDOT with certification, from a professional engineer registered in Pennsylvania, indicating that the designs comply with PennDOT's criteria and are adequate to support the loads specified therein.

After acceptance by the PennDOT, the manufacturer will not be required to submit design calculations or structural drawings on a project-by-project basis, except for signal supports which exceed the standard structure loadings indicated herein. For these special designs, a submission of design calculations, structural drawings and the professional engineer's certification must be made for each different support.

Shop drawings will be required for all traffic signal supports on each project.







MAST ARM LENGTH			S	IGNAI	LS			MAX Y					
(ft)		Μ	Ν	0	Р	Q	R	S	Т	U	V	Y	(ft)
0.10	W	70				123					39	87	5.2
0-10	Α	8.76				8.82					7.48	10.50	5.2
	W	70				123	39				39	106	6.6
	А	8.76				8.82	7.48				7.48	21.33	0.0
>10-15		OR											
	W	70				123					39	106	95
	А	8.76				8.82					7.48	21.33	7.5
>15-20	W	97	70			123	39				39	106	6.6
>15-20	А	13.89	8.76			8.82	7.48				7.48	21.33	0.0
>20-25	W	97	70			123	39	39			39	106	85
>20-23	А	13.89	8.76			8.82	7.48	7.48			7.48	21.33	0.5
	W	97	70	97		123	39	39			39	106	85
	А	13.89	8.76	13.89		8.82	7.48	7.48			7.48	21.33	0.5
>25-30		i	-	i			OR	i	i	-	i	i	i
	W	97	70			123	39	39			39	106	13.5
	А	13.89	8.76			8.82	7.48	7.48			7.48	21.33	15.5
>30-35	W	97	70	97		123	39	39	39		39	106	10.8
/ 50 55	А	13.89	8.76	13.89		8.82	7.48	7.48	7.48		7.48	21.33	10.0
	W	97	70	70	97	123	39	39		39	39	106	79
	А	13.89	8.76	8.76	13.89	8.82	7.48	7.48		7.48	7.48	21.33	1.5
		n		r	n		OR	n	r	-			
>35-40	W	97	70	70	70	123	39	39			39	106	10.8
255 40	А	13.89	8.76	8.76	8.76	8.82	7.48	7.48			7.48	21.33	10.0
		ŀ	<b>-</b>	i			OR	i	i	<b>-</b>	i	i	·
	W	97	70	97		123	39	39	39		39	106	157
	Α	13.89	8.76	13.89		8.82	7.48	7.48	7.48		7.48	21.33	13.7

 Table 20-1

 MAST ARM - STANDARD STRUCTURE LOADING

MAST ARM LENGTH			S	IGNAI	LS		SIGNS						MAX Y	
(ft)		Μ	Ν	0	Р	Q	R	S	Т	U	V	Y	(ft)	
	W	97	70	70	97	123	39	39		39	39	106	12.0	
	А	13.89	8.76	8.76	13.89	8.82	7.48	7.48		7.48	7.48	21.33	12.8	
		OR												
> 40, 45	W	97	70	70	70	123	39	39			39	106	157	
>40-43	А	13.89	8.76	8.76	8.76	8.82	7.48	7.48			7.48	21.33	13.7	
		OR												
	W	97	70	97		123	39	39	39		39	106	20.7	
	А	13.89	8.76	13.89		8.82	7.48	7.48	7.48		7.48	21.33	20.7	
	W	97	70	70	97	123	39	39		39	39	106	177	
	А	13.89	8.76	8.76	13.89	8.82	7.48	7.48		7.48	7.48	21.33	1/./	
		OR												
> 45 50	W	97	70	70	70	123	39	39			39	106	20.7	
>45-50	А	13.89	8.76	8.76	8.76	8.82	7.48	7.48			7.48	21.33	20.7	
	OR													
	W	97	70	97		123	39	39			39	106	20 5	
	А	13.89	8.76	13.89		8.82	7.48	7.48			7.48	21.33	28.3	
	W	97	70	70	97	123	39	39		39	39	106	27.0	
	А	13.89	8.76	8.76	13.89	8.82	7.48	7.48		7.48	7.48	21.33	21.9	
							OR							
> 50, 60	W	97	70	70	70	123	39	39			39	106	20.9	
>30-00	А	13.89	8.76	8.76	8.76	8.82	7.48	7.48			7.48	21.33	50.8	
							OR							
	W	97	70	97		123	39	39			39	106	20 7	
	А	13.89	8.76	13.89		8.82	7.48	7.48			7.48	21.33	38./	

W= Load in lb  $A=Area in ft^2$ 

Note:

For standard structure loading, place indicated signals and signs beginning at the furthermost point on the arm and then proceeding toward the shaft in accordance with the dimensions shown on Figure B-3 and Publication 148, TC-8801.

#### Table 20-2

## LOADS AND PROJECTED WIND AREAS FOR TRAFFIC SIGNAL HEADS

LENS SIZE – in ALL SECTIONS	SIGNAL CONFIGURATION <sup>(1)</sup>	SIGNAL SECTIONS EACH DIRECTION	DIRECTIONS	LOAD - Pound (lb) WITHOUT BACKPLATE <sup>(2)</sup>	WIND AREA - Square feet (ft <sup>2</sup> ) WITHOUT BACKPLATE $^{(3),(4)}$	LOAD - Pound (lb) WITH BACKPLATE <sup>(2)</sup>	WIND AREA - Square feet (ft <sup>2</sup> ) WITH BACKPLATE 5 in BORDER <sup>(3),(5)</sup>	WIND AREA - Square feet (ft <sup>2</sup> ) WITH BACKPLATE 8 in BORDER <sup>(3),(5)</sup>
8	А	3	1	45	2.40	48	5.97	8.79
8	А	4	1	55	3.19	59	7.46	10.69
8	А	5	1	58	3.99	69	9.17	12.46
8	В	3	2	82	2.40	88	5.97	8.79
8	С	3	2	84	5.12	90	8.69	11.51
8	В	4	2	101	3.19	109	7.42	10.69
8	С	4	2	103	6.82	111	11.09	14.32
8	В	5	2	110	3.99	131	9.17	12.46
8	D	3	3	120	5.12	129	8.69	11.51
8	E	3	3	120	7.84	129	11.41	14.23
8	D	4	3	147	6.82	159	11.09	14.32
8	E	4	3	147	10.45	159	14.72	17.95
8	F	3	4	156	7.84	168	11.41	14.23
8	F	4	4	193	10.45	209	14.72	17.95
12	А	3	1	66	4.17	70	8.76	12.23
12	А	4	1	84	5.55	89	11.04	15.09
12	А	5	1	90	6.94	97	13.89	17.90
12	В	3	2	121	4.17	129	8.76	12.23
12	С	3	2	123	8.82	131	13.41	16.88
12	В	4	2	155	5.55	165	11.04	15.09
12	С	4	2	157	11.75	167	17.24	21.29
12	В	5	2	179	6.94	189	13.89	17.90
12	D	3	3	178	8.82	190	13.41	16.88
12	E	3	3	178	13.47	190	18.06	21.53
12	D	4	3	227	11.75	242	17.24	21.29
12	E	4	3	227	17.95	242	23.44	27.49
12	F	3	4	233	13.47	249	18.06	21.53
12	F	4	4	299	17.95	318	23.44	27.49
12PED	A	2	1	43	2.77	-	-	-
12PED	C	2	2	86	6.93	-	-	-
18PED	Α	1	1	40	2.47	-	-	-
18PED	C	1	2	80	5.14	-	-	-

NOTES:

(1) Refer to Figure 20-4, Traffic Signal Configurations and Designations.

(2) A one-way 8 in lens section is 9 lb without attachment hardware and backplate. A one-way 12 in lens section is 15 lb without attachment hardware and backplate.

(3) The area for an 8 in lens section without backplate is based on a 10 in height by a 11.5 in width, and the area for a 12 in lens section without backplate is based on a 13.5 in height by a 14.8 in width.

(4) The area for a 2-section pedestrian signal assumes a 14.1 in height and a 14.1 in width for each section. The area of a 1-section pedestrian signal assumes a 18.9 in height and a 18.9 in width.

(5) Values in *shaded area* are generally not used.

